



om:

Gilmore, Tyler J [Tyler.Gilmore@pnnl.gov]

nt:

Thursday, March 06, 2014 3:08 PM Bayer, MaryRose; McDonald, Jeffrey

To: Cc:

Greenhagen, Andrew; Appriou, Delphine; Spane, Frank A

Subject:

Calculations of Critical Pressure

Attachments:

Final-FAS-Nicot-EGS-FutureGen[1].xlsx

Molly and Jeff,

In response to Molly's request for our calculations using the Nicot method, attached is an explanation and spreadsheet with the calculations.

The attached spread sheet, shows calculations of AoR critical pressure calculations based on Equations 7 and 9 of the Nicot et al. (2009). The 3 Nicot test case example calculations are also provided to demonstrate correspondence (or lack thereof) with calculation results presented in Nicot's paper. It should be realized that the assumptions and pressure gradient conditions considered by Nicot et al. (2009) are not necessarily correspondent to normal basin settings/conditions like the FutureGen site, where an existing initial/ambient pressure gradient condition exists that would support upward flow potential from the injection reservoir to the base (or in proximity the base) of the lowermost USDW. Given these reservations, critical pressure calculations based on Nicot's equations 7 and 9 provided an estimate value of 13.4 and 13.8 psi, respectively for FutureGen site conditions. It should be noted that this calculated critical pressure does not take into account the observed hydraulic head conditions at the FutureGen site, which indicate that under ambient and indicate that under ambient of the lowermost USDW.

Tyler

## Nicot et al. (2009) input parameters

Fgen Properties

Gravity 9.80665 m/s^2

Top of Injection Formation 3904 ft depth

Base of USDW 1942 ft depth

Injection Formation TDS 47,000 TDS

Borehole Range of Salinity 3.7-43.3 g/L

Reservoir Density 1.0331 kg/L

USDW Density 0.999014 kg/L

Density of Reservoir fluid at USDW conditions 1.034 kg/L

fluid density difference at base of USDW,  $\rho_i$ - $\rho_u$  0.03236 kg/L

Observed Temp for base of St. Peter

81.48 °F

Projected Pressure for base of St. Peter

806.39 psi

Salinity of St. Peter reservoir fluid

3730 ppm

fluid density of St. Peter reservoir fluid at Obs. T, Proj. P, and salinity

1.00164 g/cm3

## 32.17405 ft/s2 3838 (Elmhurst)

based on a "rounded average"

Mt. Simon - St. Peter salinity

Obs. T, Projected P, and salinity for Mt. Simon Top

freshwater density at STP conditions

see St. Peter T, P conditions below

kg/L

Nov. 2013 Schlumberger fluid temp. survey
Projected value from linear regression of MDT, packer test, and geon
Kelley et al. (2012)
http://www.csgnetwork.com/water\_density\_calculator.html

Earlougher 1977

depths are ft bgs Kelley et al. 2012

http://www.csgnetwork.com/water\_density\_calculator.html
Earlougher 1977
http://www.csgnetwork.com/water\_density\_calculator.html

nechanical test results

T = 97.99°

F, P = 1712.47 psi, TDS = 47,000 ppm

Examples	California Site
Top Inject. Res., z <sub>i</sub>	2277
USDW Base, z <sub>u</sub>	1215
Depth Diff., $\Delta z = z_i - z_u$	1062
TDS Inject. Res.	20
TDS USDW	0.5
Initial Borehole Salinity Range	0.5 - 20
USDW Density at USDW Conditions, ρ <sub>υ</sub>	
Res. Density at USDW TP Conditions, p <sub>iu</sub>	
Lambda Density Grad. of Res.@ Constant TDS, $\lambda_{piu} = (\rho_{iu} - \rho_i)/\Delta z$	-1.16E-05
Epsilon Initial Density Grad.; $\varepsilon = (\rho_i - \rho_u)/\Delta z_i$	3.75E-07
Final Density Diff. at USDW Base, p <sub>iu</sub>	0.0118
Final Density Diff. at USDW Base, $ ho_{iu}$	0.7359
Nicot Equation	Equation 9
Max. Admiss. Press.	0.58
Max. Admiss. Press.	8.412
Max. Admiss. Press.	0.058
Nicot Equation	Equation 7
Max. Admiss. Press.  Max. Admiss. Press.	3.046
Max. Admiss. Press.	0.021
Nicot Equation / Verification	
Right-Side Eqn	2073.82
Critical Pressure, $\Delta P_c$	2073.82
Critical Pressure, ΔP <sub>c</sub>	2.0738E-03
Critical Pressure, ΔP <sub>c</sub>	0.30
Critical Pressure, ΔP <sub>c</sub>	0.02
Nicot Equation 9 Verification	6.065.00
λ - ε, summation	-6.36E-03
Right-Side Eqn	5.67E+04
Critical Pressure, ΔP <sub>c</sub>	56669.04
Critical Pressure, $\Delta P_c$	5.6669E-02
	ס מי
Critical Pressure, $\Delta P_c$ Critical Pressure, $\Delta P_c$	8.22

<sup>\*</sup> Believe Nicot is off by one decimal place and 0.021 bar is the correct value

Texas Site 1	Texas Site 2	
2500	2500	m
700	700	m
1800	1800	m
60	60	g/L
0.5	0.5	g/L
0.5 - 20	0.5 - 20	g/L
		kg/L
		kg/L
		kg/L
-1.10E-05	-1.10E-05	kg m/L
-3.81E-06	-6.98E-06	kg m/L
0.0379	0.03222	kg/L
2.3637	2.0094	lb/ft <sup>3</sup>
2000		y
5.6	5.15	bar
81.221	74.694	psi
0.560	0.515	Mpa

Conversions/Con	stants		
	from	mutiplier	⊤to
kg/	/L · ft/s²	1.94032	lb/ft <sup>3</sup>
kg/	L→ m/s²	6.365879469	lb/ft³
	ft <sup>2</sup>	144	in² —
	⊪⊪рg	62.3664	lb/ft3
	kg	2.204623	lb 💮
	kg/L	62.3664	lb/ft3
	MPa	145.0377	lb/in²
Garleno miles <del>e</del>	MPa	1.00E-06	Pa
	Pa	1.45E-04	lb/in²
	bar	14.50377	lb/in <sup>2</sup>
	m	3.28084	ft
	e g	9.80665	m/s²
	- B	32.17405	ft/s²
e sanda kang kalenda di dilak Kapad Japan da Holan Rabiga	Ptw	0.999014	kg/L
	m³	1000	L

bar psi Mpa

k g/m s<sup>2</sup> Pa MPa Ib/in<sup>2</sup> bar

Examples	FutureGen Calculations
Top Inject. Res., z <sub>i</sub>	1189.94 m
USDW Base, z <sub>u</sub>	591.92 m
Depth Diff., $\Delta z = z_i - z_u$	598.02 m
TDS Inject. Res.	47 g/L
TDS USDW	3.7 g/L
Initial Borehole Salinity Range	3.7 - 47 g/L
USDW Density at USDW Conditions, ρ <sub>u</sub>	1.0016 kg/L
USDW Density at freshwater STP Conditions, ρ <sub>ufw</sub>	0.9990 kg/L
Res. Density at USDW TP Conditions, Piu	1.0340 kg/L
Res. Density at Reservoir TP Conditions, $ ho_i$	1.0331 kg/L
Lambda Density Grad. of Res.@ Constant TDS, $\lambda_{piu} = (\rho_{iu} + \rho_i)/\Delta z$	-1.52E-06 kg/Lm
Epsilon Initial Density Grad., $\epsilon = (\rho_i - \rho_u)/\Delta z$	5.26E-05_kg/L m
Final Density Diff. at USDW Base, ρ <sub>iu</sub>	0.0324 kg/L
Final Density Diff. at USDW Base, ρ <sub>iu</sub>	2.0182 lb/ft <sup>3</sup>
Nicot Equation 7	
Right-Side Eqn	92249.36 k g/m s <sup>2</sup>
Critical Pressure, $\Delta P_c$	92249.36 Pa
Critical Pressure, $\Delta P_c$	9.2249E-02 MPa
Critical Pressure, $\Delta P_c$	13.38 lb/in²
Critical Pressure, $\Delta P_c$	0.92 bar
Nicot Equation 9	
λ - ε, summation	-1.62E-02 kg/L m
Right-Side Eqn	$9.49E+04 \text{ kg/m s}^2$
Critical Pressure, ΔP <sub>c</sub>	94861.23 Pa
Critical Pressure, ΔP <sub>c</sub>	9:49E-02 MPa
Critical Pressure, $\Delta P_c$	13.76 lb/in <sup>2</sup>
Critical Pressure, ΔPc	0.95 bar

Conversions/Constants	
from	mutiplier to
kg/L•ft/s′	1.94032 lb/ft <sup>3</sup>
kg/L · m/s	2 6.3659 lb/ft <sup>3</sup>
ft	<sup>2</sup> 144 in <sup>2</sup>
PER	3 62.3664 lb/ft3
ke	g 2.2046 lb
kg/l	62.3664 lb/ft3_
MP	a   145.0377 lb/in² -
Мра	a 1.00E+06 Pa
ba	r 14.50377 lb/in²
r de la companya de	a 3.28084 ft
	g = 9.80665 m/s <sup>2</sup>
	g 32.17405 ft/s <sup>2</sup>
$ ho_h$	" 0.999014 kg/L
m	3 1000 L